

# Discovery

# Speed control of induction motor by using advanced non linear techniques and comparison

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# **ABSTRACT**

The main objective of this paper is to control the speed of the induction motor. The speed can be controlled by scalar control and vector control. Vector control separately regulates the "torque" and "flux" producing components of the motor stator current and is readily suited to implementation with a constant switching frequency. Triggering pulses to the switches of the motor are generated with PWM, Hysteresis based and P+Resonant (PR) controller. The performance of the machine is tested by simulation studies. The results shows the superior performance of the PR controller.

Index Terms—Induction Motor, Speed control, field orientation, PWM Inverter, hysteresis, P+Resonant (PR), vector drive, Matlab/simulink.

 $L_r$ 

Rotor inductance

List of S	ymbo	ls
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Ls Stator inductance Stator leakage inductance  $L_{ls}$ Mutual inductance Rotor leakage inductance

	ANALISIS	ARTICLE			
$R_s$	Stator resistance		$U_{sd}$ , $U_{sq}$	$U_{sd}$ , $U_{sq}$ dq-axis component of the stator voltages	
$R_{r}$	Roto	r resistance	i <sub>sd</sub> , i <sub>sq</sub>	dq-axis components of the stator currents	
$R_{c}$	Core resistance		$i_{s\alpha}$ , $i_{s\beta}$	$\alpha\beta$ -axis component of the stator currents	
$\omega_{\text{r}}$	Rotor speed		ψτα, ψτα	$\alpha\beta\text{-axis}$ component of the stator fluxes	
$\omega_{\text{sl}}$	Slip frequency		J	moment of inertia of rotor	
$\omega_{\text{e}}$	Elect	rical speed	$T_e$	Electrical Torque	
Р	Pole	number	$T_L$	Load Torque	
U <sub>sα</sub> , U	$J_{s\beta}$ α β-axis comp	onent of the stator voltages	δ	Rotor flux angle	

#### 1. INTRODUCTION

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Induction motors are the most common motors used in industrial motion control systems, as well as in main powered home appliances. Simple and rugged design, low-cost, low maintenance and direct connection to an AC power source are the main advantages of induction motors. Induction motors are easier to design than DC motors, the speed and the torque control in induction motors is difficult and complex [12].

There are two methods to control the speed. They are scalar control and vector control. Scalar control of ac drives produces good steady state performance but poor dynamic response. This performance is due to deviation of air gap flux linkages from their set values. This variation occurs in both magnitude and phase. Vector control (or field oriented control) offers more precise control of ac motors compared to scalar control. The superior performance of the vector control makes it more popular and suitable to high performance drives e.g. robotic actuators, centrifuges, servos, etc.[3]

The control and speed estimation of induction motor drive are more complex than those of DC drives, and this complexity increases substantially if high performances are demanded. The induction motor drive system is state variable, nonlinear with internal coupling effect. The stability analysis of induction motor is very complex. The simulation study in matlab/simulink is very useful to investigate the performance of induction motor drive, particularly when a new control technique is developed.

The simulation results show the performance of induction motor drive. Vector or field oriented control (FOC) of induction motor for a PWM voltage-fed inverter identifies the synchronously rotating flux axis from the induction motor and calculate the flux magnitude and rotor flux angle. The control voltages  $u_{s\alpha}$ ,  $u_{s\beta}$  controls the currents  $i_{s\alpha}$ ,  $i_{s\beta}$  to control speed and torque[3],[8].

#### 2. PRINCIPLES OF VECTOR CONTROL FOR A THREE-PHASE INDUCTION MOTOR

#### 1. Dynamic Model Of Vector Controlled Induction Motor

The vector control principle on induction motor takes advantages of transforming the variables from physical three-phase abc to stationary reference frame ( $\alpha\beta$ ) [1]. The mathematical model of induction motor as differential equations of five state variables presented in ( $\alpha\beta$ ) stationary reference frame is written in equation (1).[4],[8].

$$\frac{di_{s\alpha}}{dt} = k_1 \cdot i_{s\alpha} + k_2 \cdot \psi_{r\alpha} + \omega_r \cdot k_3 \cdot \psi_{r\beta} + k_4 \cdot u_{s\alpha}$$

$$\frac{di_{s\beta}}{dt} = k_1 \cdot i_{s\beta} + k_2 \cdot \psi_{r\beta} - \omega_r \cdot k_3 \cdot \psi_{r\alpha} + k_4 \cdot u_{s\beta}$$

$$\frac{d\psi_{r\alpha}}{dt} = k_5 \cdot \psi_{r\alpha} + (-\omega_r) \cdot \psi_{r\beta} + k_6 \cdot i_{s\alpha}$$

$$\frac{d\psi_{r\beta}}{dt} = k_5 \cdot \psi_{r\beta} + (-\omega_r) \cdot \psi_{r\alpha} + k_6 \cdot i_{s\beta}$$

$$\frac{d\omega_r}{dt} = \frac{L_m}{L_r J} (\psi_{r\alpha} i_{s\beta} - \psi_{r\beta} i_{s\alpha}) - \frac{1}{J} T_L$$

$$(1)$$

Where  $i_{s\alpha}$ ,  $i_{s\beta}$ ,  $\psi_{r\alpha}$ ,  $\psi_{\beta\alpha}$  and  $\omega_r$  are the state variables and  $u_{s\alpha}$ ,  $u_{s\beta}$  are the input variables and  $k_1$ ,  $k_2$ ,  $k_3$ ,  $k_4$ ,  $k_5$ ,  $k_6$  are the constants and these constant parameters are directly given in matlab/simulink .M file.

$$k_{1} = -\frac{R_{s}L_{r}^{2} + R_{r}L_{m}^{2}}{L_{r}w}$$

$$k_{2} = \frac{R_{r}L_{m}}{L_{r}w}$$

$$k_{3} = \frac{L_{m}}{w}$$

$$k_{4} = \frac{L_{r}}{w}$$

$$k_{5} = -\frac{R_{r}}{L_{r}}$$

$$k_{6} = R_{r}\frac{L_{m}}{L_{r}}$$

$$w = \sigma L_{r}L_{s} = L_{r}L_{s} - L_{m}^{2}$$

$$(2)$$

From the above equation (1) and (2) the mathematical model of induction motor model is design in Matlab/Simulink as shown in Fig. 1.

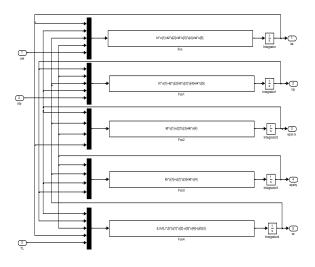


Figure 1 Induction motor model Block in Matlab/Simulink

# 3. CONTROL STRATEGIES

A. Vector Control induction motor with PWM Inverter control

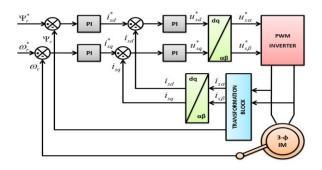


Figure 2 Vector control Induction Motor Block with PWM Inverter-fed controller

Vector or field oriented control (FOC) of induction motor for a PWM voltage-fed inverter identifies the synchronously rotating flux  $\psi_{r\alpha}$ ,  $\psi_{r\beta}$  and stator currents  $i_{s\alpha}$ ,  $i_{s\beta}$  of induction motor and calculate the rotor flux magnitude, rotor flux angle gama and  $i_{dq}$  currents from the transformation block [2], [8].

The flux magnitude  $\psi_r$  and rotor speed  $\omega_r$  are compared with reference flux and speed, and then the error flux and error speed is generated. The generated error flux and speed is given to the PI controller then the stator currents  $i_{sd}$ \*, $i_{sq}$ \* are generated and these currents are compared with actual currents from the induction motor is  $i_{sd}$ ,  $i_{sq}$  and then the error currents will be generated. To generate a voltages  $u_{sd}$ \*, $u_{sq}$ \* the error currents are given to PI controller. The voltages  $u_{sd}$ \*, $u_{sq}$ \* are transformed to  $\alpha\beta$ -axis stationary voltages to three phase abc voltages [5]. The three phase abc voltages are compared with triangular carrier signal.[6]

when carrier signal is less than or equal to reference signal then +ve pulses are generated and when the carrier signal is greater than or equal to reference signal then –ve pulses are generated this pulses are used to trigger the thyristors of inverter in order to control line side of inverter.

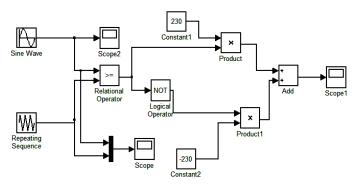


Figure 3 PWM Inverter Logic Block in Matlab/Simulink for 1phase

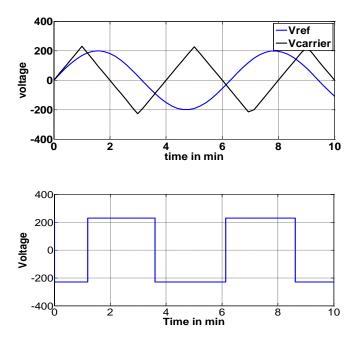


Figure 4 Output pulses for single phase PWM inverter block in Matlab/simulink.

The output voltages of the PI controllers are transformed from a rotating to a stationary frame using the Park transformation. The commanded signals of the stator voltage are sent to the pulse width modulation (PWM) block. Then the voltages are generated like as show in Fig. 4 for single phase inverter logic. The rotor flux magnitude is calculated from the following equation (3) and the transformation block is shown in Fig.

$$\left|\psi_{r}\right| = \sqrt{\psi_{r\alpha}^{2} + \psi_{r\beta}^{2}}\tag{3}$$

From the above equation (3) the transformation block is designed in Matlab/Simulink as shown in below Fig. 5

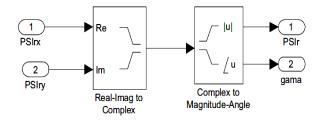


Figure 5 Transformation block in Matlab/Simulink

2. Vector Control Induction Motor with Three-Phase Hysteresis controller

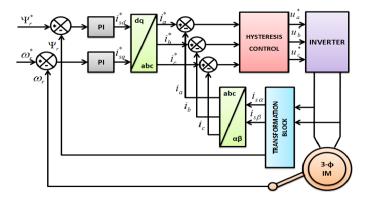


Figure 6 Vector control Induction Motor Block with Hysteresis controller

The three-phase stationary frame currents  $i_a^*$ ,  $i_b^*$  and  $i_c^*$  are calculated from the  $i_d^*$  and  $i_q^*$  currents. The three-phase reference currents are compared with actual currents and then given to hysteresis band as shown in Fig. 7. The hysteresis upper band limit is 0.1 and lower band limit is -0.1. The hysteresis controller output is control voltages  $U_a$ ,  $U_b$  and  $U_c$  which are given to the vector control of induction motor [6], [7].

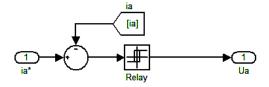


Figure 7 Hysteresis band for single phase in Matlab/Simulink

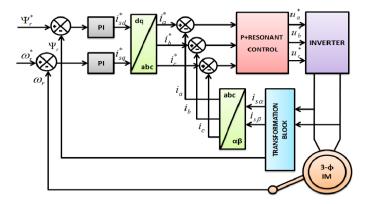


Figure 8 Vector control Induction Motor Bock with PR controller

# C. Vector Control induction motor with Stationary Frame Proportional Resonant(PR) controller

In PR control strategy the three-phase reference currents  $i_a^*$ ,  $i_b^*$  and  $i_c^*$  are compared with actual currents coming from the induction motor  $i_a$ ,  $i_b$ , and  $i_c$  ,then the error currents will produce and these error currents are given to PR controller then the controllable voltages  $u_a^*$ ,  $u_b^*$ ,  $u_c^*$  will be produce and these voltages are given to vector control induction motor.[6][7]

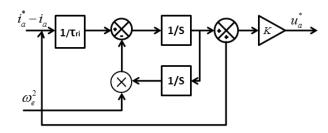


Figure 9 Stationary frame PR controller Block in Matlab/Simulink

$$\begin{bmatrix} u_{a}^{*} \\ u_{b}^{*} \\ u_{c}^{*} \end{bmatrix} = k \left( 1 + \frac{s}{\tau_{ri} (s^{2} + \omega_{e}^{2})} \right) \begin{bmatrix} i_{a}^{*} - i_{a} \\ i_{b}^{*} - i_{b} \\ i_{c}^{*} - i_{c} \end{bmatrix}$$
(4)

Where k is the current loop proportional gain,  $T_{ri}$  is the current loop integrator reset time constant.

The slip frequency  $\omega_{sl}^*$  is generated from  $i_{qs}^*$  from equation and this slip speed is added with speed signal  $\omega_r$  to generate frequency signal  $\omega_e$ .

$$\omega_{sl}^* = \frac{L_m R_r}{\widehat{\psi}_r L_r} i_{qs}^* \tag{5}$$

In PR controller the error current with current loop integrator reset time constant is compared with square of electrical speed  $\omega_e$  is to generate voltages.

# 4. SIMULATION RESULTS

The following figures representing simulation results for PWM inverter-fed IM, Hysteresis controller and P+Resonant (PR) control technique. Fig. 10(a), (b) and (c) shows the speed performance, and Fig. 11(a), (b) and (c) shows the torque characteristics for PWM inverter-fed IM, Hysteresis controller and P+Resonant (PR) control technique

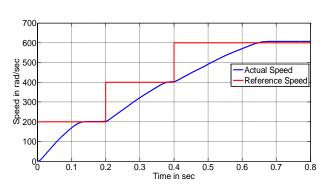


Figure 10(a). Speed response for PWM inverter-fed IM

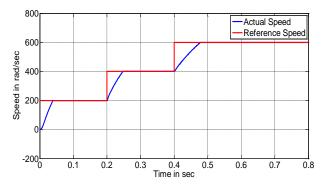
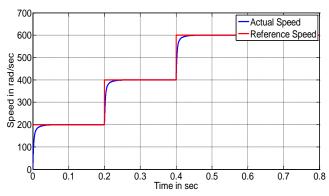
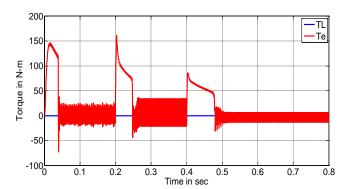


Figure 10(b). Speed response for Hysteresis controller-fed IM



**Figure 10**(c). Speed response for PR controller-fed Induction Motor



**Figure 11**(b). Torque characteristics for Hysteresis controller-fed IM

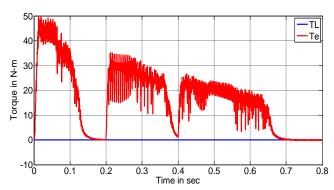


Figure 11(a). Torque characteristics for PWM inverter-fed IM

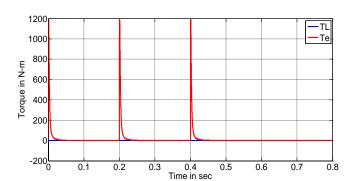


Figure 11(c). Torque characteristics for PR controller-fed IM

# **Input Parameters of Induction Motor**

SI.No:	Induction Motor Data				
	Parameters	symbol	Value		
1.	Rotor Resistance	R <sub>r</sub>	0.39Ω		
2.	Stator Resistance	R <sub>s</sub>	0.19Ω		
3.	Core Resistance	R <sub>c</sub>	0.2 Ω		
4.	Rotor Inductance	L <sub>r</sub>	1mH		
5.	Stator Inductance	Ls	0.61mH		
6.	Mutual Inductance	L <sub>m</sub>	0.4mH		
7.	Rotor leakage Inductance	L <sub>lr</sub>	0.6mH		
8.	Stator Leakage Inductance	L <sub>ls</sub>	0.21mH		
9.	Moment of Inertia	J	0.0226kg m <sup>2</sup>		
10.	Base Frequency	F	50Hz		

#### 5. CONCLUSION

The simulation results shows that the performance characteristics of Proportional Resonant (PR) vector control induction motor is improved that is the reduction in torque ripple and speed performance is improved when compared to PWM Inverter-fed vector control induction motor and hysteresis current control-fed vector control induction motor. Application of vector control induction motor with Proportional Resonant (PR) generate significant benefits in performance improvement and energy saving in home and industrial appliances.

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